

## ACTIVATION OF HIGH FLUX TEST MODULE SAMPLE HOLDER AFTER IFMIF-DONES OPERATION

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Nuclear safety assessment in nuclear fusion devices relies on the Monte Carlo method based neutron transport calculations. This paper presents information about the calculation results of the activities and dose rates caused by neutron irradiation for the structural materials of the high flux test module sample holder of IFMIF-DONES. The neutron induced activities and dose rates at shutdown were calculated by means of the FISPACT-2010 code with data from the EAF-2010 nuclear data library. Neutron fluxes and spectra were obtained with MCNP neutron transport calculations. The activities and dose rates were calculated at the end of irradiation of the assumed device operation scenario for cooling times of 0 s – 1000 year. In addition, radionuclides with contribution of at least 0.5% to the total value of activation characteristics at the previously mentioned cooling times were identified. After the operation, the most active radionuclide is  $^{55}\text{Fe}$ , with an activity share ranging from 30% (M200) to 63% (M8), and at the end of the prediction it accounts for 86% of the total activity. The highest dose rates at the end of irradiation are attributed to  $^{56}\text{Mn}$  radionuclide.  $^{54}\text{Mn}$  and  $^{60}\text{Co}$  are the most dominant radionuclides during intermediate and long cool-down periods.

**Keywords:** IFMIF-DONES, fusion, neutron irradiation, MCNP, FISPACT

### 1. Introduction

Nuclear energy is a relatively clean energy source in terms of carbon footprint in comparison to widely used fossil fuels. There are two main nuclear processes that can result in net energy gain: fusion and fission. Although nuclear fission based technologies currently play an important role in the energy market, they have issues with radiation protection, nuclear waste storage and limited fuel resources. Nuclear fusion offers the alternative that mitigates the formerly mentioned issues to more manageable levels [1]. On the other hand, nuclear fusion technologies face their own

challenges, for example: fusion devices are very complicated and achieving sustainable fusion on earth is not an easy task [2]. In order to ensure safety of fusion devices, most times Monte Carlo method based neutron transport calculations are performed. The Monte Carlo method is based on simulation of individual particle histories in complex environment. Particle histories follow the established laws of physics; however, the outcome is decided by random events that are described by probability distributions [3].

There are many possible fusion reactions that result in energy release. At the moment, the most promising and feasible for the controlled thermonuclear

process are reactions between hydrogen isotopes (deuterium and tritium) and helium [4]. Most of the energy released during D-T fusion reactions is carried by neutrons. Self-sustaining nuclear fusion can only be achieved if certain particle densities, temperatures and confinement times are present. The cross-section of the D-T reaction is the highest at the selected plasma temperature (around 100 million degrees) [5].

Based on the preliminary engineering project of IFMIF (International Fusion Materials Irradiation Facility), the European Union has proposed a plan for the development of the DONES (DEMO-Oriented Neutron Source) nuclear fusion facility [6]. IFMIF-DONES neutrons will be generated during the Li (d, xn) reaction by liquid lithium target bombardment with deuterium ions (up to 40 MeV). The device will be capable to produce energetic neutrons and will employ acceleration current (125 mA) in order to procure high neutron flux [ $>10^{18} \text{ m}^{-2} \text{ s}^{-1}$ ] in order to achieve exposure conditions relevant to nuclear fusion for material

testing and qualification. Neutron exposure in material samples will result in structural damage and activation. Activation will not be limited to samples as a large part of the facility will be exposed to neutron irradiation as well. The highest neutron intensity will be at the Test Cell (TC) (Fig. 1) [7] and its High Flux Test Module (HFTM) [8] where material samples are held (for more details see Figs. 2, 3) [9]. Estimation of activation in TC and HFTM is critical for the operation and maintenance of the device as it could lead to radiological hazards for staff and sensitive electronics.

## 2. Computational methods

The MCNP (Monte Carlo n-particle) particle transfer code was developed by the Los Alamos National Laboratory in the United States. It was programmatically written using the FORTRAN and C programming languages.

For neutron spectrum calculations the neutron transport equation must be solved:

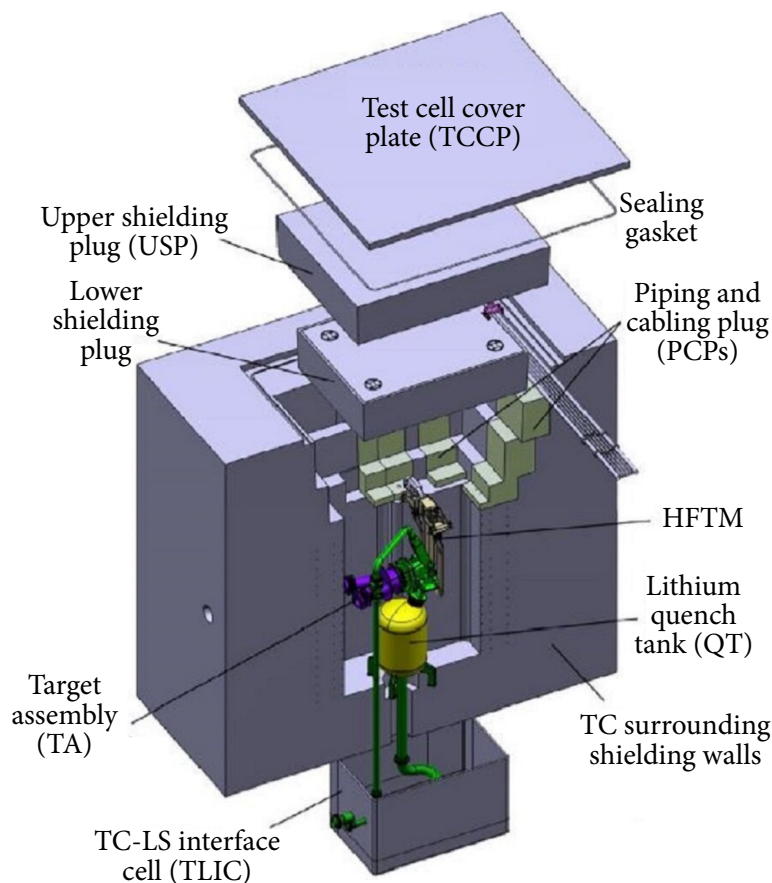


Fig. 1. Model of the Test Cell including the High Flux Test Module [7].

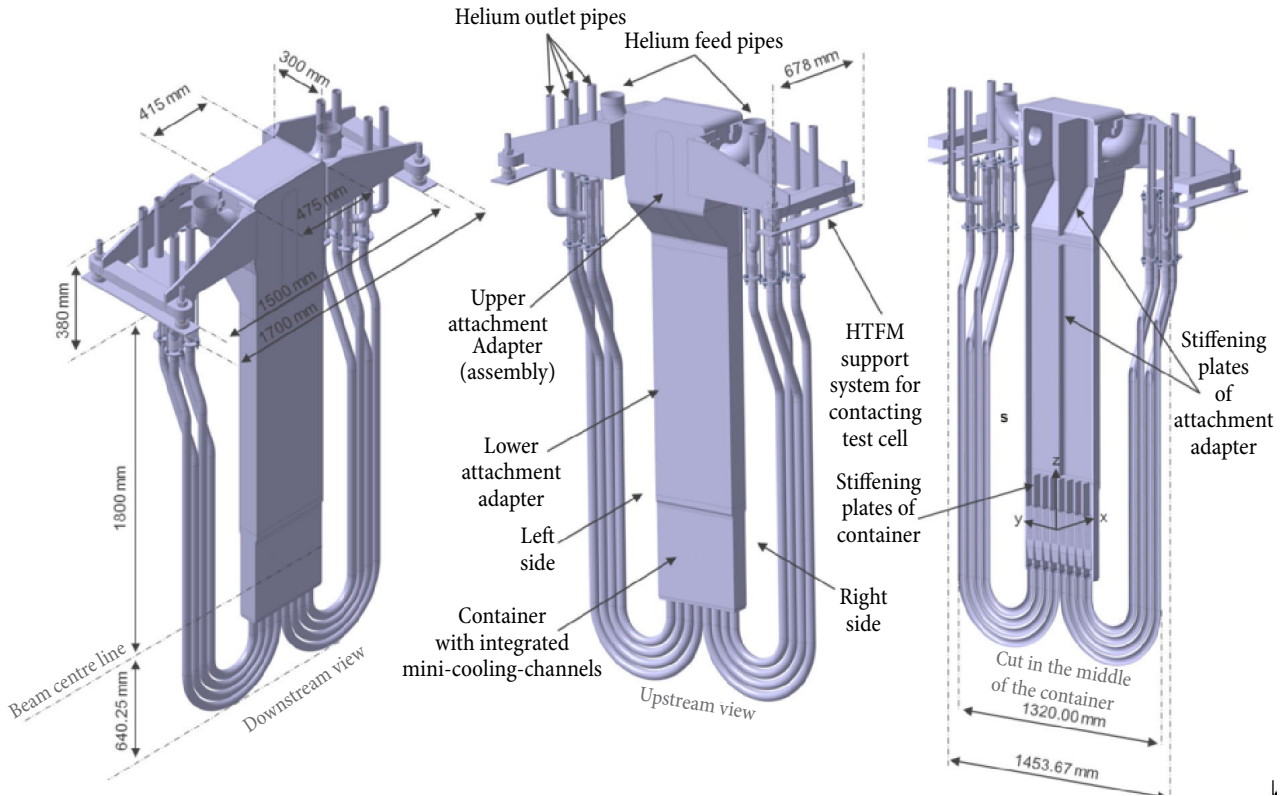


Fig. 2. IFMIF-DONES High Flux Test Module. From left to right: a downstream view, an upstream view, a downstream view but cut in the middle of the container with the global coordinate system of IFMIF-DONES [8].

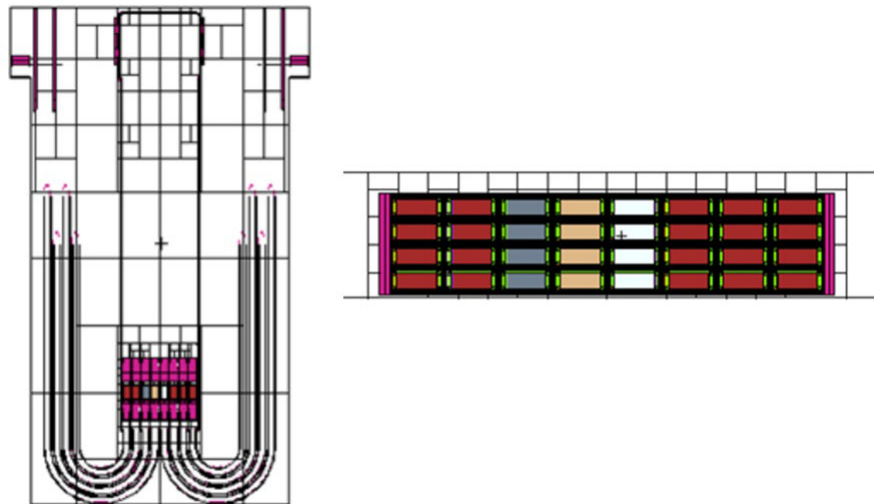


Fig. 3. MCNP model of the IFMIF-DONES HFTM sample holder.

$$\begin{aligned}
 & \frac{1}{v} \frac{\partial \phi}{\partial t} + \Omega \nabla \phi + \Sigma_t \phi(r, E) = \\
 & \int_0^\infty dE' \int_{\Omega'} \Sigma_s(r, z') f(r, E' \rightarrow E, \Omega' \rightarrow \Omega) \phi(r, E', \Omega', t) d\Omega' \\
 & + \frac{\chi(E)}{4\pi} \int_0^\infty dE' \int_{\Omega'} v \Sigma_f(r, E') \phi(r, E', \Omega', t) d\Omega' \\
 & + S(r, E, \Omega, t).
 \end{aligned} \tag{1}$$

The MCNP uses three processes to solve neutron transport equations:

- (1) using the probability distribution determines the source parameters;
- (2) neutron location, energy and direction tracking;
- (3) data recording and analysis of results [10].

The FISPACT-2010 is describing the amounts of various nuclides in materials after given irradiation

steps. It can be achieved by solving the Bateman differential equations

$$\frac{dN_i(t)}{dt} = -N_i(\lambda_i + \sigma\phi) + \sum_j N_j(\lambda_{ij} + \sigma_{ij}\phi) + S_i, \quad (2)$$

$$S_i = \sum_k N_k \sigma_k^f \phi Y_{ik}, \quad (3)$$

where  $N_i$  is the amount of nuclide  $i$  at time  $t$ ,  $\lambda_i$  is the decay constant of nuclide  $i$ ,  $\lambda_{ij}$  is the decay constant of nuclide  $j$  producing  $i$ ,  $\sigma_i$  is the total cross section for reaction  $i$ ,  $\sigma_{ij}$  is the reaction cross-section for reaction  $j$  producing on  $i$ ,  $\sigma_k^f$  is the fission cross-section for reactions on actinide  $k$ ,  $\phi$  is the neutron flux,  $S_i$  is the source of nuclide  $i$  from fission, and  $Y_{ik}$  is the yield of nuclide  $i$  from the fission of nuclide  $k$ . The set of the previously mentioned differential equations is solved using the Sidell method. Due to the dependence on the duration of irradiation and cooling sequences only nuclides with sufficiently long half-lives are calculated by this method, and nuclides with shorter half-lives are considered to be in equilibrium [11].

### 3. Calculation results

Neutron spectra (Fig. 4) were determined by using the IFMIF-DONES neutron source and geometry model. Neutron fluxes and energy distribution were obtained for the structure of the HFTM sample holder. All neutron transport calculations were

done by using MCNP5 with the JEFF-3.1.2 [12] nuclear library.

Activation analysis and radionuclide identification were performed with the FISPACT-2010 code with the EAF-2010 nuclear data library [13].

JEFF-3.1.2 is the general purpose fusion and fission nuclear data library, while EAF-2010 is the nuclear data library optimized for fusion applications. A concise structure of EAF-2010 enables a shorter computation duration.

For activation calculations the IFMIF-DONES irradiation scenario was employed that assumes facility operation for 10 years. Each year consists of 345 days of continuous irradiation and 20 days of downtime representing the maintenance work. Specific activities and dose rates were obtained and dominant radionuclides were identified for HFTM. Only radionuclides contributing more than 0.5% to the total value after any of the considered time interval are presented.

Activities and dose rates were calculated for the HFTM sample holder structure, which consists of 14 materials used for structural integrity and thermal insulation: SS316L (N), EUROFER 97 and several compounds such as M40 (EUROFER 97 | AISI 321 | MgO | NiCr 80/20 | INNOBRAZE ML 442), M200 (Silica Aerogel, Si (OCH<sub>3</sub>)<sub>4</sub>) and M8 (Fe, Cr, W, Mn, and some other elements). 11 of the investigated materials were iron based (see Table 1).

The specific activity dependence on time is shown in Fig. 5. At the end of irradiation, <sup>55</sup>Fe is the most active radionuclide and represents 30%

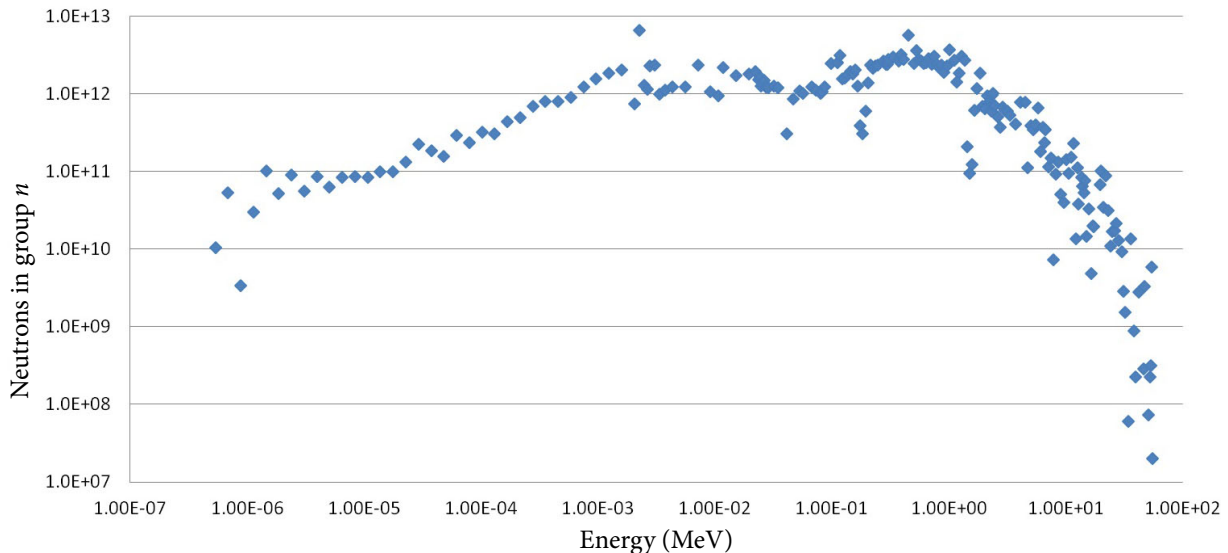


Fig. 4. Neutron spectrum.

Table 1. Chemical composition of the investigated materials.

M1	%	M2	%	M3	%	M5	%	M8	%	M30	%
Fe	62.974	Fe	65.4	Fe	47.442	Fe	61.645	Fe	87.974	Fe	84.777
Cr	18	Cr	16.998	O	33.035	Cr	18.5	Cr	9.5	Cr	9.155
Ni	12.5	Ni	11.998	Ca	7.103	O	13	W	1.199	Na	3.634
Mo	2.699	Mo	2.499	Ti	5.434	Mn	2.499	Mn	0.6	W	1.155
Mn	2	Mn	2	Si	2.575	Mn	2	V	0.25	Mn	0.578
Cu	1	Si	0.75	Al	2.348	Cu	1	Ta	0.15	V	0.241
Si	0.5	Nb	0.1	Mg	0.934	Si	1	C	0.12	Ta	0.144
Other	0.322	Other	0.255	Other	1.129	Other	0.357	Other	0.19	Other	0.295

M31	%	M32	%	M33	%	M40	%	M200	%
Fe	84.857	Fe	84.94	Fe	85.02	Fe	74.9	Fe	26.6663
Cr	9.163	Cr	9.172	Cr	9.181	Cr	10.65	O	24.1705
Na	3.544	Na	3.449	Na	3.358	Ni	7.723	C	17.2439
W	1.156	W	1.158	W	1.159	Mg	2.298	Si	10.2879
Mn	0.579	Mn	0.579	Mn	0.58	O	1.52	Cr	7.4234
V	0.241	V	0.241	V	0.242	W	0.916	Ni	5.9955
Ta	0.145	Ta	0.145	Ta	0.145	Mn	0.686	H	4.3041
Other	0.295	Other	0.296	Other	0.296	Other	1.283	Other	3.8842

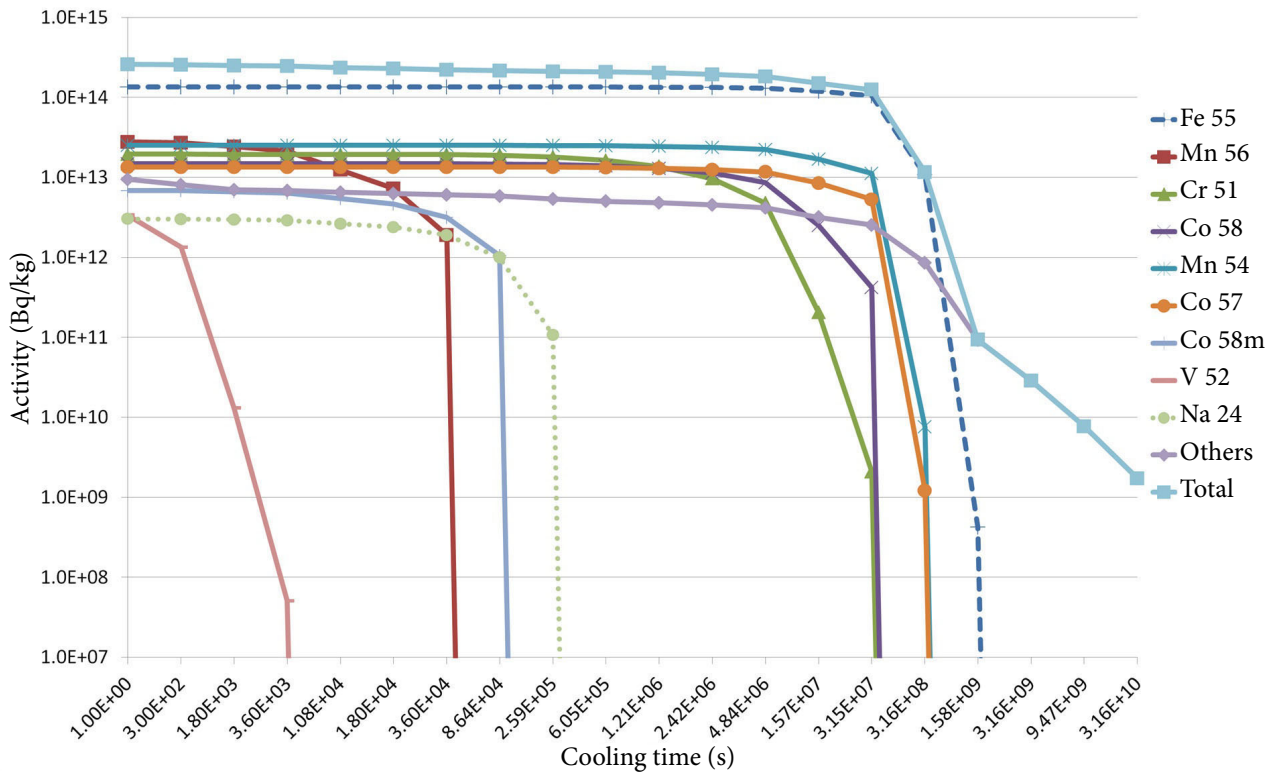


Fig. 5. Specific activity at HFTM for M40.

(M200) to 63% (M8) of the total activity. In addition to this, the contribution of <sup>54</sup>Mn and <sup>56</sup>Mn is 7% (M200) to 13% (M8) of total activities. Although the half-life of the <sup>55</sup>Fe iron isotope is

relatively long (half-life is 2.734 yr), it remains the most relevant isotope for almost all prediction time period. A more detailed analysis of the obtained results shows that <sup>55</sup>Fe is produced from

the  $^{54}\text{Fe}$  neutron capture reaction with gamma radiation as a by-product. The neutron capture reaction is responsible for  $^{56}\text{Mn}$  production from  $^{55}\text{Mn}$ .

The main radionuclides that are gamma radiation sources are presented in Fig. 6. As we can see, the largest contribution to the equivalent dose rate

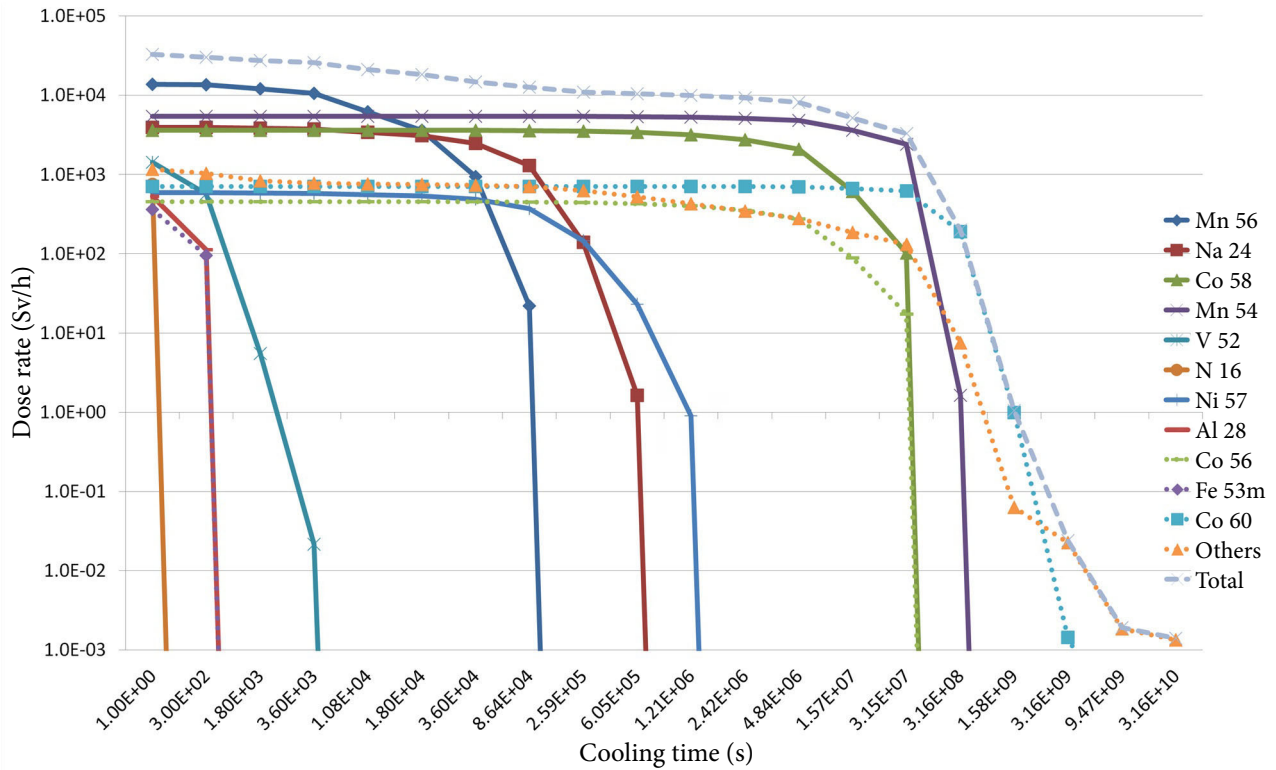


Fig. 6. Dose rate at HFTM for M40.

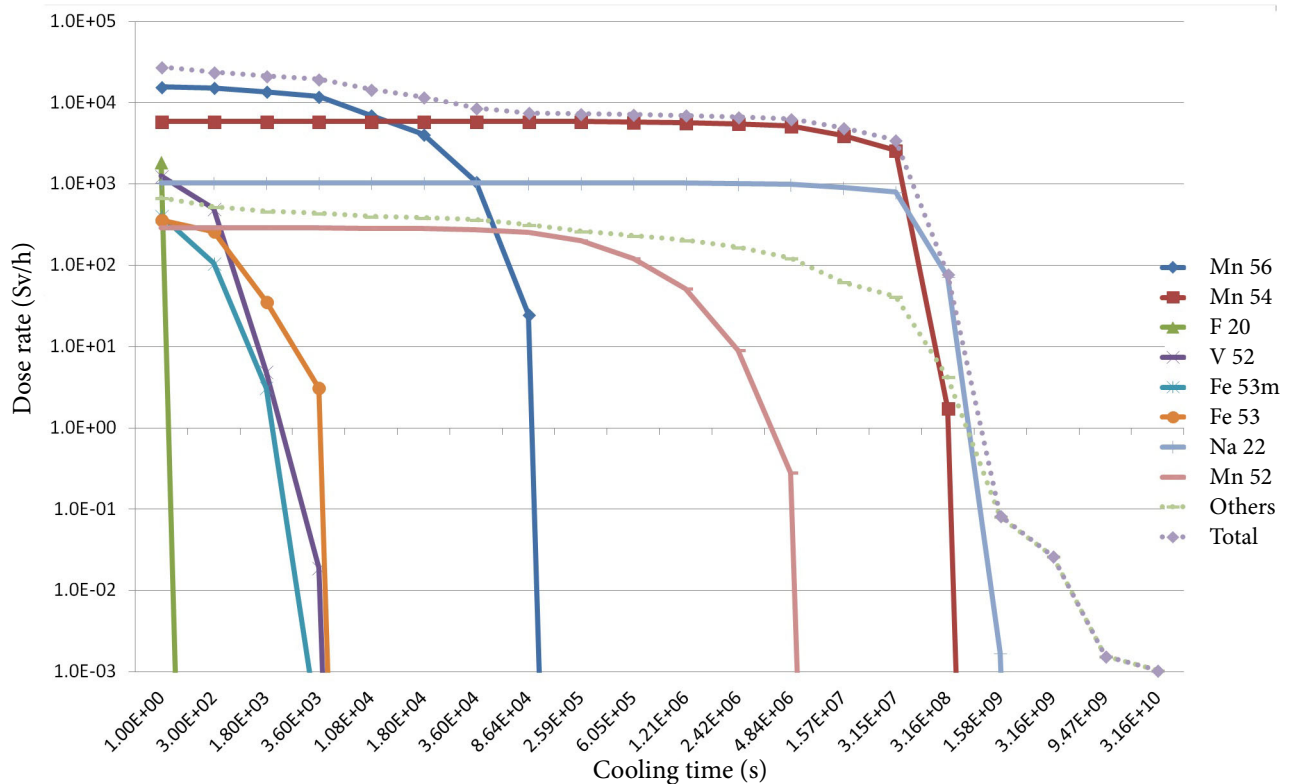


Fig. 7. Specific dose rate at HFTM for EUROFER 97.

is provided by  $^{56}\text{Mn}$ , but due to its short half-life (2.64 h),  $^{58}\text{Co}$  (half-life is 70.86 d.) and  $^{54}\text{Mn}$  (half-life is 312.2 d.) are relevant for longer times. From 10 to 100 years due to the long half-life (5.273 m),  $^{60}\text{Co}$  emits almost 100% of the total dose.

In Fig. 7, we can see that the main dominant radionuclides are the same as in the material in Fig. 6; however, in Fig. 7 there are some differences in radionuclides responsible for the total dose rate. The main contributors are  $^{56}\text{Mn}$  and  $^{54}\text{Mn}$ , while  $^{60}\text{Co}$  is insignificant and amounts to less than 0.5% of the total dose rate.

As seen in Fig. 8, in the first second after the end of irradiation, the increase in the iron content increases the activity of the  $^{55}\text{Fe}$  isotope

fraction in the material. The highest activity (272.8 TBq/kg) is reached in the AISI SS316L material with 65% iron content.  $^{51}\text{Cr}$  has the greatest influence on SS316L. For the activity of M40 (concentration of Fe in material is ~75%), in addition to  $^{51}\text{Cr}$ ,  $^{56}\text{Mn}$  and  $^{54}\text{Mn}$  are also significant sources.

Figure 9 depicts the iron percentage and related specific activity values present for 181 days of the observation time. During this time period, the influence of iron activation products (mainly  $^{55}\text{Fe}$ ) increases with regard to the total specific activities. It should also be noted that the activity of iron isotopes ( $^{55}\text{Fe}$  and  $^{53}\text{Fe}$ ) ranges from 65% (M200) to 86% (M8). The most active substance

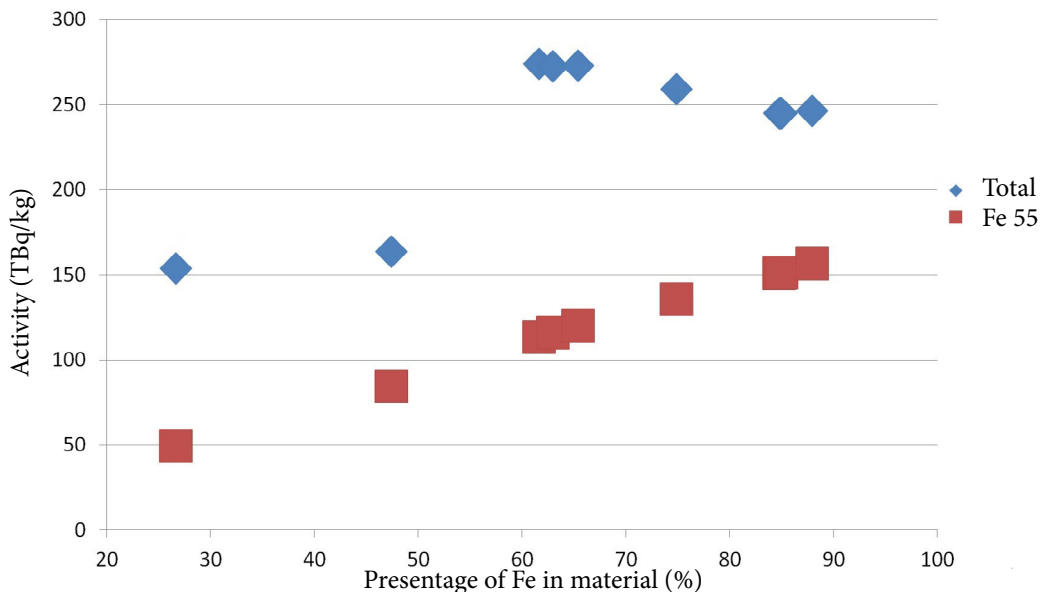


Fig. 8. Specific activity dependence on the iron content in the material (1 second of cooling).

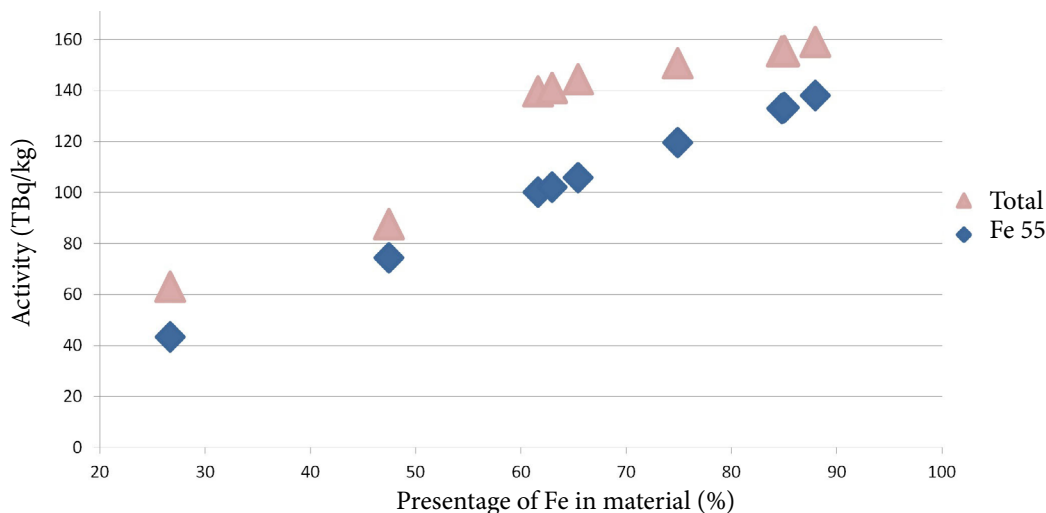


Fig. 9. Specific activity dependence on the iron content in the material (181 days of cooling).

is M8, containing 87.97% of iron, and has a total activity of 159.1 TBq/kg after 181 d.

#### 4. Summary

The objective of this study was to calculate the activities and dose rates in the HFTM sample holder structure at the IFMIF-DONES induced by neutron irradiation. Subsequent activities and dose rates at shutdown were calculated by means of the FISPACT-2010 code using the irradiation scenario specified for the IFMIF-DONES. After the end of irradiation, the activities and dose rates were calculated at the cooling time of 0 and 1 s, 5 and 30 min, 1, 3, 5 and 10 h, 1 and 3 days, 2, 4 and 8 weeks, 181 days, 1, 10, 100, 300 and 1000 years.

The investigation of the iron based materials shows that the total dose rate values range from  $2.5 \cdot 10^4$  to  $4 \cdot 10^4$  Sv/h within the first second after the end of irradiation and drops to  $1.05 \cdot 10^{-3}$ – $5.92 \cdot 10^{-2}$  Sv/h, respectively, after 1000 years of cooling.

The specific activity of  $^{55}\text{Fe}$  in the metal samples ranges from  $4.92 \cdot 10^{13}$  to  $1.57 \cdot 10^{14}$  Bq/kg at the first second of the cooling time and from  $1.54 \cdot 10^8$  to  $4.95 \cdot 10^8$  Bq/kg after 50 years of the cooling time. The highest activity value belongs to M8. After 50 years, no activity of  $^{55}\text{Fe}$  was observed.

The total specific activity in the metal samples ranges from  $1.63 \cdot 10^{14}$  to  $2.74 \cdot 10^{14}$  Bq/kg at the first second of the cooling time and from  $1.72 \cdot 10^8$  to  $5.21 \cdot 10^{10}$  Bq/kg after 50 years of the cooling time. The highest activity values belong to M8.

At 0 second of the cooling time, the most active radionuclide is  $^{55}\text{Fe}$ : its activity ranges from 30% (M200) and 63% (M8) of the total activity up to 86% at the end of the observation.  $^{56}\text{Mn}$  is the radionuclide emitting the highest doses, but it decays fast and due to the longer half-life the dominant nuclides at the end of the cooling time are  $^{54}\text{Mn}$  and  $^{60}\text{Co}$ .

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#### References

- [1] K. Tokimatsu, H. Hondo, Y. Ogawa, K. Okano, K. Yamaji, and M. Katsurai, Energy analysis and carbon dioxide emission of Tokamak fusion power reactors, *Fusion Eng. Des.* **48**(3–4), 483–498 (2000), [https://doi.org/10.1016/S0920-3796\(00\)00157-5](https://doi.org/10.1016/S0920-3796(00)00157-5)
- [2] L.J. Qiu, *Fusion Energy and Its Application* (Science Press, Beijing, 2008).
- [3] L.W. Dunn and J.K. Shultis, *Exploring Monte Carlo Methods* (Elsevier Science, 2011).
- [4] W. Yican, *Fusion Neutronics* (Springer Singapore, 2017).
- [5] Y.C. Wu, E. Stevens, K. Kim, D. Maisonnier, A. Kalashnikov, K. Tobita, D. Jackson, C. Alejaldre, D. Perrault, D. Panayotov, et al., Summary of the 1st International Workshop on Environmental, Safety and Economic Aspects of Fusion Power, *Nucl. Fusion* **56**(12), 127001 (2016).
- [6] *Overview of IFMIF-DONES and Testing of Materials for DEMO* (2016), [https://elamatscience.ifj.edu.pl/slides/Ibarra\\_slides.pdf](https://elamatscience.ifj.edu.pl/slides/Ibarra_slides.pdf)
- [7] K. Tian, B. Ahedo, F. Arbeiter, G. Barrera, Ł. Ciupiński, T. Dézsi, J. Horne, D. Kovács, J. Molla, F. Mota, et al., Overview of the current status of IFMIF-DONES test cell biological shielding design, *Fusion Eng. Des.* **136**(A), 628–632 (2018).
- [8] Q. Yuefeng, F. Arbeiter, U. Fischer, and F. Schwab, IFMIF-DONES HFTM neutronics modeling and nuclear response analyses, *Nucl. Mater. Energy* **15**, 185–189 (2018).
- [9] A. Ibarra, F. Arbeiter, D. Bernardi, M. Capelli, A. Garcia, R. Heidinger, W. Krolas, U. Fischer, F. Martin-Fuertes, G. Micciché, et al., The IFMIF-DONES project: preliminary engineering design, *Nucl. Fusion* **58**(10), 105002 (2018).
- [10] X-5 Monte Carlo Team, *MCNP – A General Monte Carlo N-particle Transport Code, Version 5* (2003).
- [11] R.A. Forrrest, *The FISPACT-2007 User Manual* (Culham Science Centre, 2007).
- [12] *The JEFF-3.1 Nuclear Data Library*, eds. A. Koning, R. Forrrest, M. Kellett, R. Mills, H. Henriksson, and Y. Rugam, JEFF Report 21 (OECD/NEA, Paris, 2006).



[13] L.W. Packer and J.-Ch. Sublet, The European Activation File: EAF-2010 decay data library (Culham Science Centre, Oxfordshire, 2010).

## DIDELIO NEUTRONŲ SRAUTO TESTAVIMO MODULIO BANDINIŲ LAIKIKLIO AKTYVUMAS PO IFMIF-DONES EKSPLOATACIJOS

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### Santrauka

Vertinant branduolių sintezės prietaisų saugumą yra atliekami neutronų pernašos lygties skaičiavimai. Dalis jų pagrįsti Monte Karlo metodu. Straipsnyje pateikiami aktyvumų ir dozės galių skaičiavimų rezultatai, kuriuos lemia neutronų apšvita IFMIF-DONES didelio neutronų srauto testavimo modulio bandinių laikiklio struktūrinėse medžiagose. Bandinių laikiklį sudaro 14 medžiagų (11-oje iš jų pagrindinis elementas yra geležis): SS316L (N), EUROFER 97, M40 (EUROFER 97 | AISI 321 | MgO | NiCr 80/20 | INNOBRAZE ML 442), M200 (Silica Aerogel, Si (OCH<sub>3</sub>)<sub>4</sub>), M8 (Fe, Cr, W, Mn ir kiti elementai). Neutronų sukelti aktyvumai ir dozės galios įrenginio eksploatavimo metu buvo apskaičiuoti

pritaikius FISPACT-2010 kodą su EAF-2010 branduolinių duomenų biblioteka. Neutronų spektras buvo gautas naudojant MCNP kodą neutronų pernašos lygties skaičiavimams. Aktyvumai ir dozės galios buvo apskaičiuotos aušimo laikams nuo 0 s iki 1000 metų. Taip pat buvo nustatyti radionuklidai, turintys mažiausia 0,5 % bendro aktyvumo vertės anksčiau minėtais aušimo laikais. Stebėjimo pradžioje geležies tipo medžiagose aktyviausias radionuklidas buvo <sup>55</sup>Fe, kurio aktyvumo dalis medžiagose svyruoja nuo 30 % (M200) iki 63 % (M8), o stebėjimo pabaigoje sudaro 86 % bendro aktyvumo. Didžiausia dozės galia pasižymi radionuklidas <sup>56</sup>Mn, o ilgesniais aušimo laiko periodais – <sup>54</sup>Mn ir <sup>60</sup>Co.